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Optimizing the Mechanical Performance of Adobe Bricks Reinforced with *Vicia faba* Plant Waste and Derived Biochar Using ANN and RSM

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Abstract

Using traditional materials, especially earthen materials and plant waste, is becoming more popular worldwide due to lower construction costs, improved thermal comfort, reduced energy use, and fewer carbon dioxide emissions. In this context, tests have been performed on a stabilized earth bricks (SEBs) made from raw earth bricks combined with *Vicia faba* waste (VW) and biochar derived from this waste (BVfW), obtained by pyrolysis at 300°C and 500°C, using a factorial design with BVfW contents ranging from 0.5 to 6 wt%. The effects of these compounds on the controlled variables were

examined using artificial neural network (ANN) techniques and response surface methodology (RSM) to assess the mechanical behavior and thermophysical properties of the bricks within a system that varies the percentage of BVW and pyrolysis temperature. The best conditions were found to be 500°C and 4% BVW content, based on the RSM desirability function and the ANN genetic algorithm. This experimental approach allows for optimizing production conditions by selecting the best parameters to create bricks with balanced strength.

Keywords: Earthen bricks; *Vicia faba*; Mechanical behavior; thermophysical properties; Optimization.

Nomenclature

VW *Vicia faba* waste

BVW Biochar derived from *Vicia faba* waste

SEBs Stabilized earth bricks

RSM Response Surface Methodology

ANOVA Analysis of Variance

CCD Central Composite Design

DF Desirability function

ANN Artificial Neural Network

MS Mean square

p-value Probability value

F-value Fisher value

SD Standard deviation

MLP Multilayer Perceptron

RMSE Root Mean Square Error

MSE Mean Square Error

R^2 Correlation coefficient

CV Coefficient of variation

AP Adequate precision

3D Three-dimensional

2D Two-dimensional

GA genetic algorithm

FS Flexural strength

CS Compressive strength

TC Thermal conductivity

DPW Date palm waste

KNN K-nearest neighbors

CKD Cement kiln dust

1. Introduction

Rising levels of greenhouse gas emissions and air pollution drive climate change, a major global issue that impacts the climate, human health, and the economy. The building sector significantly contributes to CO₂ emissions and consumes a large share of non-renewable energy [1]. Implementing strategies to reduce CO₂ emissions is essential [2]. Energy-saving planning and measures to lower potential emissions must be prioritized to promote a reduction in CO₂ emissions [3]. Reusing materials, minimizing waste, and developing sustainable products are some recent strategies aimed at lowering carbon dioxide emissions and their harmful environmental effects [4-6]. In this context, many research studies have been conducted to reduce energy consumption related to air conditioning and heating systems, especially through improving wall thermal insulation and material choice [7,8]. In this context, using raw earth bricks made of bio-based composite materials is a particularly appealing approach. These minimally processed, low-carbon bricks not only decrease building energy requirements but also significantly reduce CO₂ emissions during construction. They are a sustainable option, especially in rural areas, due to their natural ability to regulate indoor temperatures, local availability, and affordability [9,10].

Given the negative environmental effects of cement use, especially regarding CO₂ emissions and energy consumption, clay bricks appear to be a viable and sustainable alternative [11]. They align fully with sustainable building

principles because they are traditionally made without complex industrial processes. Although there was a decline with the rise of commercial materials, clay, a natural substance mined directly from the earth, has been used for thousands of years in construction and remains popular in poorer countries [12]. The geographical context influences its physical and chemical properties as well as how it is used, with local agricultural resources often affecting the choice of additives. Due to their minimal environmental impact and ability to support more eco-friendly construction, raw earth bricks are increasingly favored in the construction industry, according to numerous studies [13,14]. According to previous research, the mechanical properties of old adobe buildings, such as their compressive and tensile strengths, range from 0.66 to 2.15 MPa and 0.12 to 0.40 MPa, respectively [15]. However, these properties can be improved in adobe stabilized with gypsum, which can achieve a bending strength of over 1.5 MPa and a compressive strength (CS) of 4.72 MPa, as proposed [16]. A study on raw earth bricks reinforced with fibers and chemical stabilizers observed similar patterns [23].

Several recent studies have examined the stabilization of raw earth using natural fibers for building purposes [17-20]. The results confirmed the positive effects of these fibers on the thermomechanical properties of the bricks. Bouhicha et al. [18] observed that if the straw content is ideal, adding straw improves CS while lowering shrinkage and hardening time. Likewise, the researchers found that the straw-reinforced specimen was more ductile than a sample without straw, and they also noted an increase in flexural strength (FS) and shear strength. Furthermore, according to Eslami et al. [21], adobe bricks reinforced with palm fibers perform better mechanically than unreinforced ones, especially in terms of tensile strength and ductility. Interestingly, a fiber percentage of 0.25% yielded the best CS, while tensile strength increased directly with fiber dosage. According to Zak et al. [22], the density of earth bricks mainly determines their CS, while hemp and flax fibers have little effect on strength but significantly alter fracture behavior.

Conversely, adding gypsum and cement tends to weaken the clay matrix, which greatly reduces CS. Adding fibers to bricks offers an effective way to improve durability and strength. Recent studies have explored various agricultural residues, such as straw, sawdust, and seaweed [23,24], demonstrating that fiber incorporation—ranging from 0.5% to 3%—can enhance flexural and compressive strengths by approximately 30%, often meeting minimum regulatory standards. However, the impact of bio-additives varies; while materials like alfalfa[25] and date palm waste[26] can significantly improve thermal insulation, they may also lead to a reduction in compressive strength if the fiber content exceeds optimal thresholds (typically 0.25% to 2%) [27,28]. Nevertheless, the stabilization of excavated soil with cement and Alfa fibers has shown that achieving high mechanical performance (up to 8.12 MPa) remains possible alongside reduced thermal conductivity [29].

Prioritizing recyclable and environmentally friendly building materials, such as biochar-based insulation and bricks, is essential for a full commitment to sustainable development [30–32]. Biochar, produced by pyrolyzing biomass, is highly useful for building materials and heat generation [33]. Its remarkable qualities—low density, low TC, and high porosity—make it a promising alternative to fossil carbon resources and an effective tool for reducing greenhouse gas emissions [34–37]. As a result, biochar significantly enhances a building's sustainability [38–40]. Recent quantitative assessments demonstrate the magnitude of this impact; for instance, incorporating 30% biochar can sequester approximately 59 kg of CO₂ per tonne of material, effectively achieving a carbon-negative footprint [41]. Furthermore, the global adoption of biochar-based strategies could theoretically mitigate up to 12% of current anthropogenic greenhouse gas emissions [42], highlighting its transformative potential in shifting the construction industry toward a durable carbon sink model [43]. Despite these benefits, this locally available resource remains underutilized in sustainable construction, where it is

produced from agricultural waste to reinforce raw earth bricks—an achievement the authors claim is a first in the field. Biochar not only increases the value of an organic by-product but also plays a key role in CO₂ sequestration, significantly reducing the carbon footprint of construction materials [44,45]. In the context of earthen construction, such as adobe, the integration of bio-additives is particularly relevant. Unlike conventional fired bricks, adobe bricks are produced without high-temperature firing, resulting in inherently low embodied energy [46]. Enhancing their thermophysical properties through bio-based stabilization—using plant aggregates or biochar—further elevates their status as a high-performance, low-carbon alternative. Recent studies suggest that such reinforcements can improve mechanical resistance and thermal insulation while effectively trapping carbon within the material matrix [47].

To maximize these advantages, new techniques such as artificial neural networks (ANN) and response surface methodology (RSM) have recently been used to optimize the traits of bio-based materials that include biochar. Several studies have demonstrated the effectiveness of digital approaches, such as heuristic frameworks, combined data sets, and K-nearest neighbors (KNN)/ANN metamodels, which have led to the use of RSM and ANN to improve mechanical performance [48,49]. Boumaaza et al. [50] studied the optimization of bio-mortars by replacing part of the cement with biochar produced from pyrolyzing *Washingtonia filifera* waste at different temperatures (300, 400, and 500°C). They examined factors affecting porosity, CS, and TC using RSM. The results show that using 1% biochar pyrolyzed at 500°C results in a TC of 0.52 W/m·K and a CS of 63.81 MPa after 28 days. Based on optimization through RSM and ANN, a ratio of 1% *Washingtonia filifera* waste pyrolyzed at 500°C enhances mechanical performance by 5% in FS, 20% in displacement, and 265% in flexural modulus [51]. Additionally, Nakkeeran et al. [52] utilized ANN and RSM to optimize the properties of Bio-Bricks made from peanut shells and cementitious

binders. When predicting dry density, CS, and water absorption, the ANN models showed exceptional accuracy ($R^2 > 0.99$). Using ANN, RSM, and Technique for Order Preference by Similarity to Ideal (TOPSIS) methods, Mebarkia et al. [53] optimized the production of low-temperature clay bricks by adding cement kiln dust (CKD). By testing various proportions of CKD (0–30%) and firing temperatures between 600°C and 900°C, they found optimal conditions—approximately 30% CKD at temperatures ranging from 800°C to 896°C—that improve the thermomechanical properties of the bricks while reducing their environmental impact.

The idea is to conceive an ecological insulation material at very low cost and which can meet the technical requirements in the building sector. Additionally, this study aimed to determine the optimal mixture of these additives to achieve the best performance. To do this, a statistical regression model was created to forecast the mechanical and thermal characteristics of stabilized earth bricks (SEBs) in conjunction with an ANN and RSM. These models take into account the *Vicia faba* waste (VW) as well as the addition of biochar derived from these waste (BVW) levels (0.5%, 0.75%, 1%, 2%, 3%, 4%, 5%, and 6%) by weight, pyrolyzed at 300°C and 500°C to the mixture. This research is novel because no previous studies have explored these two methods to predict the mechanical and thermophysical properties of bricks containing biochar. Nevertheless, to the authors' knowledge, no research has been conducted on using VW and biochar BVW to produce bricks. Thus, the innovative application of VW and BVW biochar makes this study remarkable.

2. Materials and methods

2.1 Materials

The *Vf*, or broad bean, is a legume widely cultivated across Algeria, especially in the Ben Djerrah region, located in the wilaya of Guelma (36°26'04.51"N 7°22'42.05"E). It is an annual plant that grows between 20 and 180 cm tall, with an upright, ribbed stem [54]. Aside from its culinary uses, this plant

produces a significant amount of agricultural waste, particularly plant fibers from the stems and pods, which can be recycled through a circular economy approach. Bean stalks are transformed using a controlled retting method designed to separate the cellulose fibers. The stems undergo spontaneous bacterial breakdown when kept submerged for around a month at a steady temperature of 30 to 35°C, releasing the fiber bundles from their plant matrix. These fibers provide a renewable and eco-friendly option for the creation of high-performance bio-based materials after being manually removed and dried (**Fig. 1**).

The *Vf* fibres were pyrolysed to obtain B*Vf* for use in this research. The pyrolysis technique, which involves heating *Vf* waste in an oxygen-poor atmosphere, is used to produce biochar from these fibers. Through this heat treatment, the biomass is transformed into a stable, carbon-rich material with a highly microporous structure, enabling effective long-term CO₂ sequestration. Following this, they were pyrolyzed for 30 minutes at temperatures of 300°C and 500°C in a sealed oven. The furnace is equipped with a vent system to allow volatile vapors from organic compounds to be released during pyrolysis. Before being used to prepare bio-adobe, the resulting biochar was processed into finer particles using a grinder and cooled in a hermetic container [50]. When used as reinforcement in raw earth bricks, the biochar produced in this manner exhibits interesting physical and chemical properties that enhance its mechanical strength and thermal performance while reducing environmental impact.

Measurements were made in accordance with the NF P 18-560 standard [55] to ascertain the grain-size distribution of the soil. Biochar derived from *Vicia faba* waste (B*Vf*) has a finer particle distribution than soil, which helps it absorb more into the clay matrix, according to the particle size study (**Fig. 2**). The soil's suitability for earthen construction is confirmed by the fact that the particle-size distribution curve completely fits within the recommended zone given by ASTM D2487 standard [56] for SEBs. A highly compact structure with

balanced porosity is indicated by the soil's specific gravity of 2520 kg/m³ and apparent density of about 1285 kg/m³. The plasticity of the soil was determined through original laboratory tests following the ASTM D4318 standard [57]. The soil was found to be quite pliable, with a plasticity index of 17% and a liquid limit of 35% according to the Atterberg limits. This classification indicates a clay fraction (particles < 2 μm) of approximately 22%, which plays a fundamental role in the binding behavior and the development of the mechanical strength of the bio-based bricks. During drying and curing, these characteristics maintain shape, compaction, and dimensional stability. At the same time, a finer particle-size distribution is seen in the BC. This implies that adding it to soil mixtures could enhance matrix uniformity and fill up interstitial spaces.

2.2. Bricks manufacturing

Adobe bricks are created by combining clay, water, biochar, and fibers from the *Vicia faba* plant (**Fig. 3**). Brick samples with BVW percentages ranging from 0.5% to 6% were pyrolyzed at 300°C and 500°C with 1% VW. After mixing the dry components for 30 minutes, the mixtures were hydrated until they reached a homogeneous plastic state suitable for optimal compaction. This consistency was carefully controlled to ensure the mixture was moist enough to prevent crumbling while remaining dry enough to avoid sticking to the mold, thus ensuring structural integrity upon demolding. The weight of the bricks is maintained at 850 g, as is that of the fibre (10 g), while the biochar content varies from 0.5% to 6% by weight, or 5 g to 60 g. This biochar is added to the clay to improve the brick's thermomechanical properties. It is produced by pyrolyzing the V_f waste at 300°C and 500°C, turning plant leftovers into a porous carbon material that can permanently trap CO₂.

Water is added to each mixture based on the biochar content, with the water-to-dry-mix ratio ranging from 23.5% (for 0.5% biochar) to 64.7% (for 6% biochar and *Vicia faba* waste). Because biochar is porous and absorbent, it needs more water to create a uniform mixture and facilitate molding, which

explains the direct relationship between biochar percentage and water amount. While excess water can affect the bricks' cohesiveness and strength, insufficient water can make the mixture less flexible.

To ensure biochar-based bricks maintain good shape, and optimal performance after hardening, water dosage must be adjusted according to the amount of biochar. This precise control allows the full benefits of biochar—especially its mechanical strength, reduced TC, and ability to sequester carbon—to be realized. Bricks made from BVW were produced following the experimental plan (**Table 1**). A total of sixteen distinct brick formulations were prepared and analyzed. These consist of eight different biochar percentages (ranging from 0.5% to 6%) combined with two separate pyrolysis temperatures (300°C and 500°C), as detailed in Table 2. Each combination represents a unique sample set, allowing for a comprehensive evaluation of the interaction between biochar dosage and thermal treatment on the bricks' properties. To ensure experimental consistency, several parameters were kept constant for all formulations: the soil type (Guelma clay), the fiber content (fixed at 1% VW or 10 g), and the total dry weight of each brick (850 g).

2.3. Mechanical and physicothermal properties

Prismatic specimens measuring $40 \times 40 \times 160 \text{ mm}^3$ were used for bending strength (FS) testing with universal testing equipment Zwick/Roell Z005 at an applied loading rate of 50 N/s in accordance with ASTM C348-14 [58]. The CS experiment was conducted using cubic samples measuring $40 \times 40 \times 40$ [59]. For each combination, a group of three specimens was tested. ASTM C642 [60] was used to measure the accessible porosity to water. From samples submerged in water (M_{water}), saturated with air (M_{air}), and dried in an oven at 90°C (M_{dry}), porosity (P) was calculated using **Equation (1)**:

$$P(\%) = \frac{(M_{\text{air}} - M_{\text{dry}})}{(M_{\text{air}} - M_{\text{water}})} \times 100 \quad (1)$$

The European standard ISO 22007-2 [61] describes the slab test process used to assess the TC of bricks. A flatbed thermal conductivity-meter with two

cooling units at both ends of a heated central element was used to measure a material's TC. Both samples were placed into the spaces within the heating and cooling units to ensure consistent heat transfer. Once the heat transfer stabilized, the coefficient of thermal transfer λ (W/m·K) of each specimen was calculated using **Equation (2)**:

$$\lambda = \frac{Q \times d}{2A(T_1 - T_2)} \quad (2)$$

Q (W) indicates the cooling unit's heating power, d (m) denotes the sample's width, A (m²) represents the thermal transfer region, and T_1 and T_2 (K) are the temperatures of the heating and cooling units, respectively.

The systematic methodology and sequential stages of this research, ranging from material preparation to predictive validation, are outlined in the framework presented in **Fig. 4**.

2.4. Mathematical Models

2.4.1. Experiment Design Using Response Surface Methodology (RSM)

RSM is a set of mathematical and statistical methods used to identify relationships between independent parameters and outcomes [62,63]. The central composite design (CCD) was employed to analyze data from bricks reinforced with B VW using the Design Expert 13 software. As shown in **Table 1**, The RSM considers two independent factors: B VW % (A) and temperature (B). The codes (-1) and (+1) indicate different levels in the experimental design, representing the minimum and maximum values assigned to the center points. Sixteen tests were performed (**Tables 2 and 3**) to establish the process conditions using the RSM/CCD approach. A second-order polynomial equation was used to calculate the compressive stress, flexural stress, and TC based on the independent variables.

$$Y = \beta_0 + \sum_1^k \beta_i X_i + \sum_1^k \beta_{ij} X_i X_j + \sum_1^k \beta_{ii} X_i^2 \quad (3)$$

In this case, Y represents the experiment's outcome (FS, CS, and TC), X_i and X_j are the independent variables, β_{ij} and β_{ii} denote the interaction effects and quadratic coefficients, respectively, and β_0 and β_1 represent the fixed and linear coefficients related to the CCD estimation.

2.4.2. Artificial Neural Network (ANN)

A practical approach for reconstructing the behavior of any nonlinear process is to use ANN modeling [64,65]. The neuronal functions of the human brain are mathematically and numerically mimicked by ANNs [53]. These networks consist of multiple interconnected artificial neurons, each employing a mathematical model to produce a single output based on all its inputs. The neural network that represents the input variables is in the input layer, the hidden layer is in the second layer, and the ANN outputs are in the final layer (output layer), forming a multilayer perceptron (MLP) architecture. The nonlinear variation in transfer (f) is usually associated with the hyperbolic type, as shown in **Equation (4)**:

$$f = \sum_{i=1}^n W_i X_i \quad (4)$$

where: W_i represents the adjusting settings, X_i for the neurons' input parameters, and n indicates the number of neurons.

In this study, three MLPs are used independently to predict FS, CS, and TC responses, respectively: 2-5-1, 2-7-1, and 2-8-1. **Fig. 5** shows the structure of the applied MLP. The input layer, the first visible layer, consists of two neurons that process the input data. The second layer, known as the hidden layer, creates a unique model after analyzing the incoming input. It has five, seven, and eight neurons for FS, CS, and TC, respectively. The output layer, which produces the final output, contains a single neuron. The weights and biases of the neurons in the ANN are adjusted during training to minimize the residual error. The Levenberg-Marquardt (LM) algorithm is used in this study to perform this optimization. The ANN outputs a value by applying activation functions to the sum of weighted inputs. The network captures

nonlinear interactions through the tanh activation functions in the hidden layers.

By calculating the difference between the predicted and observed responses of the network, error ratios evaluate the accuracy of an ANN model. The current ANN model is assessed using the correlation coefficient (R^2). The mean square error (MSE) and root mean square error (RMSE) are two key metrics [66,67]. They are expressed as follows:

$$R^2 = \frac{\sum_{i=1}^n ((\text{Predicted}_i - \text{Actual}_i))}{\sum_{i=1}^n ((\text{Predicted}_i - \text{Actual}_i)^2)} \quad (5)$$

$$\text{RMSE} = \sqrt{\frac{\sum_{i=1}^n ((\text{Predicted}_i - \text{Actual}_i)^2)}{n}} \quad (6)$$

$$\text{MSE} = \frac{\sum_{i=1}^n ((\text{Predicted}_i - \text{Actual}_i)^2)}{n} \quad (7)$$

2.4.3. Applying Genetic Algorithms (GAs) and Artificial Neural Networks (ANN)

Algorithms designed to mimic the evolution of the human genetic system are called genetic algorithm (GA) approaches. To address both linear and nonlinear problems, GA explores all regions and use potential areas by applying mutations, crossovers, and selections to the population members. The GA-ANN model combines two methods: the ANN and the GA.

3. Results and discussions

3.1. Mechanical and thermophysical properties

Fig. 6a illustrates how FS changes with BVW concentration and pyrolysis temperature. The graph shows a non-linear trend: strength steadily increases with biochar content until reaching a maximum at 4%, then declines. The strength rises from 0.52 MPa (0.5%) to 1.33 MPa (4%) at 300°C, then drops to 1.03 MPa (6%). This rise is more prominent at 500°C, reaching 1.47 MPa (4%), before decreasing to 1.13 MPa (6%). This pattern indicates that moderate biochar addition enhances the material's density and internal

cohesion, likely by strengthening the clay matrix and plugging pores. However, the increase in strength despite rising porosity (**Fig. 6c**) suggests that mechanical performance is not governed by void volume alone, but rather by the quality of the interface between the biochar and the soil matrix.

Temperature plays a decisive role in this mechanism through the chemical and physical transformation of the fibers. At 500°C, the more complete carbonization of the B V/W increases the surface roughness and the functional groups of the biochar particles, fostering stronger mechanical interlocking with the clay. Furthermore, at this temperature, the partial thermal activation of clay minerals (dehydroxylation) initiates a pre-sintering process, which compensates for the increased porosity by creating more rigid mineral bridges [68,69]. However, strength decreases more rapidly ($\geq 5\%$), possibly due to excess carbon particles disrupting the structure and increasing porosity. Temperature also plays an important role: bricks fired at 500°C are stronger than those fired at 300°C at all percentages, implying that higher temperatures promote component reactivity. The FS of the bricks increased from 0.50 MPa for the reference mortar to 0.52 MPa and 0.54 MPa for bricks with B V/W pyrolyzed at 300°C and 500°C, respectively, when 0.5% B V/W was added. This slight increase suggests that even low levels of biochar can improve load distribution and reduce microcracks, enhancing the matrix.

This finding aligns with research by [70,71], which demonstrated that adding biochar or plant fibers improves mechanical properties up to a certain point, beyond which dispersion becomes uneven and porosity increases. These patterns also match the results of research conducted by Kumar et al. [72], who examined the effect of adding biochar, made up of 90% sawdust and 10% rice husks, to cement paste. Their study shows that FS increases with 3% biochar but decreases at 5% and 10%, indicating an optimal threshold. Conversely, the formulation with 4% B V/W and 500°C promotes the recovery of organic waste and reduces environmental impact while maintaining competitive mechanical strength (1.47 MPa).

Fig. 6b shows how CS of bricks changes with fire temperature and the percentage of BVW. The results indicate that strength gradually increases as biochar content rises to an optimal level of 4%, reaching 4.16 MPa at 300°C and 4.41 MPa at 500°C before decreasing beyond that point. This pattern suggests that biochar helps reinforce the clay matrix, likely due to improved compaction, lower porosity, and positive interactions between carbon particles and mineral binders. It is essential to note that while porosity increases constantly (**Fig. 6c**), CS also increases up to 4%. This decoupling confirms that the "bridging effect" and the internal friction provided by the biochar particles outweigh the negative impact of the voids up to this threshold. The shift from 300°C to 500°C induces a more advanced decomposition of organic volatiles within the fibers, leaving a more stable carbon skeleton that acts as a structural micro-reinforcement.

The effect of temperature is also evident: bricks fired at 500°C have slightly higher strength than those fired at 300°C at each addition rate, indicating better densification and more effective sintering[73,74]. At 500°C, the removal of chemically bound water from the clay matrix improves the chemical affinity between the mineral phase and the biochar surfaces. The best formulations at 4% BVW and 500°C show a 100% increase over the reference brick (2.20 MPa), highlighting the potential of biochar as a mechanical reinforcement. These findings agree with Kumar et al. [72], who observed that adding 3% biochar to cement pastes increased their CS, but it decreased at 5% and 10% due to uneven dispersion and excess porosity. By adding BVW in moderation and controlling pyrolysis temperatures, the bricks' FS and CS can be maximized, while organic waste is recycled in line with sustainable construction principles.

As shown in **Fig. 6c**, the results for porosity as a function of burning temperature and BVW percentage reveal a clear pattern: porosity increases with biochar content, regardless of temperature. The improved formulations reach up to 8.11% at 300°C and 8.24% at 500°C for 6% BVW, while the

reference brick without biochar has a porosity of 4.96%. The porous nature of biochar itself, which introduces additional voids and changes the material's compactness when incorporated into the matrix, explains this steady increase. The effect is minimal (≈ 6.4 – 6.9%) at low levels (0.5–1%), but above 2%, porosity nears 7.5%, indicating matrix saturation and less uniform dispersion. Temperature also influences porosity, though to a lesser extent. For each addition rate, the values at 500°C are slightly higher than those at 300°C. This is attributed to the thermal degradation of residual hemicellulose and cellulose at 500°C, which increases the internal vesicularity of the biochar, and the potential onset of clay dehydroxylation, which generates additional micro-pores. The findings of Kumar et al. [72], which indicate that adding biochar to cementitious materials increases porosity—especially at rates above 5%—are consistent with this trend.

The insulating effect of this material is supported by the TC data, which show a consistent decrease in TC as the biochar percentage increases (**Fig. 6d**). At 300°C and 500°C, the improved formulations reach values as low as 0.36 W/(m·K) from 5% BVW, while the reference brick without biochar has a TC of 0.69 W/(m·K). This reduction is due to biochar's low density and porous structure, which restrict heat transfer through the matrix. TC decreases from 0.69 to 0.36 W/(m·K) between 0 and 6% BVW at 300°C, a drop of over 48%. At 500°C, the decline is similar even though the initial value is slightly higher (0.75 W/(m·K) at 0.5%).

Bricks can be optimized for sustainable and bioclimatic construction by using BVW, which enhances their thermal efficiency and reduces conductivity without significantly compromising their mechanical properties. The BVW-based formulation (4%, 500°C) exhibits a porosity of 7.96%, an FS of 1.47 MPa, a CS of 4.41 MPa, and a TC of 0.39 W/(m·K), all of which align with the latest research findings on biobased bricks. These results support your material's competitiveness for non-load-bearing applications while also reducing carbon emissions and improving thermal insulation.

The thermal and mechanical properties of the optimized BVW-based formulation (4%, 500 °C) align with the functional requirements for sustainable and bioclimatic construction. Specifically, the measured compressive strength of 4.41 MPa exceeds the 4.14 MPa (600 psi) threshold established by ASTM C129 [75] for non-load-bearing masonry units. When compared to the reference control specimen (plain soil), which exhibited a compressive strength of 2.20 MPa, a flexural strength of 0.50 MPa, and a thermal conductivity of 0.69 W/(m·K), the optimized brick demonstrates a 100% increase in compression, a 194% gain in flexural strength, and a 48% reduction in thermal conductivity. Combined with a porosity of 7.96% and a low thermal conductivity of 0.39 W/(m·K), these results confirm that BVW optimization significantly enhances insulation performance while effectively doubling the mechanical resistance required for high-performance non-structural applications.

Fig. 7 shows the fracture surface of stabilized earth bricks containing *Vicia faba* plant fibres. A ductile failure mode is observed, in which the fibres act as structural bridges across the cracks. Unlike a brittle fracture, which would be clean and smooth, the fibres here 'stitch' the earthen matrix together, increasing the material's ability to absorb energy and resist tensile stress after cracking. The incorporation of biochar complements this structure by densifying the matrix and improving adhesion at the fibre-earth interface. By filling the pores, biochar reduces areas of weakness, allowing for more efficient transmission of stresses to the fibres and thus optimizing the overall mechanical performance of the adobe.

3.2. Response surface methodology (RSM) for flexural strength (FS), compressive strength (CS) and thermal conductivity (TC)

A CCD was performed to assess how process parameters influence the prediction of flexural CS and TC for different brick types. Because of their higher correlation coefficients (R^2), adjusted R^2 , and anticipated R^2 , the quadratic models meet the previously set selection criteria. The second-

degree polynomial equations, which predict the responses for FS, CS, and TC based on the CCD experimental design, provide the derived model equations, corresponding to **Equations (8)-(10)**, respectively. These equations effectively explain how the independent parameters relate to the responses, according to the results of the Analysis of Variance (ANOVA).

$$\text{Flexural strength} = 1.3212 + 0.2543 \times \text{BVfW} + 0.0401 \times T + 0.0201 \times \text{BVfW} \times T - 0.4825 \times \text{BVfW}^2 + 0.0000 \times T^2 \quad (8)$$

$$\text{Compressive strength} = 4.1601 + 0.4013 \times \text{BVfW} + 0.0556 \times T + 0.0294 \times \text{BVfW} \times T - 1.4103 \times \text{BVfW}^2 + 0.0000 \times T^2 \quad (9)$$

$$\text{Thermal conductivity} = 0.3989 - 0.1428 \times \text{BVfW} + 0.0197 \times T - 0.0244 \times \text{BVfW} \times T + 0.1199 \times \text{BVfW}^2 + 0.0000 \times T^2 \quad (10)$$

An ANOVA was conducted for each response model to determine the nature and type of relationships among the parameters (**Table 4**). The ANOVA's Fisher values (F -values) for the FS, CS, and TC models are 116.11, 188.84, and 75.56, respectively, indicating that these models are highly significant. Additionally, the significance of the model terms is confirmed by the p -values, which are less than 0.0001 and well below 0.0500. The qualities of CS, FS, and TC are greatly affected by terms A, B, and A^2 in the current model. For the FS, CS, and TC models in this analysis, the Adequate Precision (AP) values—indicating that the signal-to-noise ratio exceeds four—are 28.6106, 35.9346, and 22.6245, respectively. These values demonstrate that the models are useful in the field of design and suggest an adequate signal.

To assess the relevance and quality of the quadratic models for biochar-based bricks, diagnostic graphs related to test datasets are also essential. The R^2 values for FS, CS, and TC, which are 97.69%, 98.56%, and 96.49%, respectively, show a strong correlation between expected and observed values, demonstrating the models' good fit to different test data. The corresponding adjusted R^2 values are 95.21%, 98.04%, and 96.85%. A reasonable agreement exists for each response when the difference between

the expected and fitted R^2 values is less than 0.2 [76]. These models can help explore the design space. The standard residual plot suggests a normal distribution of errors, with most values aligned on the right (**Figs. 8a-10a**). As seen in **Figs. 8b-10b**, the correlation between actual and predicted values forms an almost perfect linear line, confirming that these quadratic models are accurate and appropriate for these materials. The experimental results closely match the predictions. As shown in **Figs. 8c-10c**, the linear pattern of residuals indicates a consistent error distribution, suggesting a typical error range with constant variance across responses [77,78]. **Figs. 8d-10d** display the residuals' trend relative to the expected results. The variables FS, CS, and TC can be reliably estimated using the regression equations provided, based on the data above. Therefore, the response models are adequate and suitable for predicting the FS, CS, and TC of bricks.

Fig. 11 shows the response surface and 3D plots of the FS, CS, and TC for the developed model. The properties of the composite bricks are significantly influenced by increasing the biochar content and pyrolysis temperature, as illustrated by the two-dimensional (2D) and 3D curves. The steady rise in FS and CS with biochar content, peaking at around 4%, indicates enhanced internal cohesion and particle adhesion. A high treatment temperature (up to 500°C), which promotes biochar carbonization and improves its compatibility with the clay matrix, supports this trend. Due to its microporous structure, biochar also increases the porosity of the bricks, which is further intensified at higher temperatures and may affect mechanical strength beyond a certain point. The graphs clearly show a decrease in TC with biochar addition, indicating its role as a thermal insulator. The optimal regions where the combined effects of temperature and biochar maximize mechanical performance while minimizing conductivity are highlighted by the 3D response surfaces. These findings align with research [79], which demonstrated that biochar treated between 300°C and 500°C improves the strength, durability, and thermal properties of building materials. Therefore,

RSM results confirm good agreement between the experimental outcomes and the predictions.

3.3. Artificial neural network (ANN)

In this study, an ANN model was used to calculate the FS, CS, and TC of bricks containing BVW. The input variables for the backpropagation multilayer ANN are temperature ($^{\circ}\text{C}$) and biochar weight (BVW%), while the recorded FS, CS, and TC values serve as the output layer. During ANN training, feedforward networks with backpropagation—a method that transforms and propagates information from the input layer to the output layer—are commonly employed. The training phase of backpropagation involves multiple steps until the smallest error rate is reached [67,80].

The MATLAB Neural Network Toolbox was used to design the ANN architecture. The input layer of the network has two neurons, while the hidden layers for FS, CS, and TC contain five, seven, and eight neurons, respectively. The final layer, called the exit layer, has a single neuron that produces the output data. Three runs of the dataset were used for testing, validation, and training. The experimental design included sixteen runs: twelve for network training (75%), two for testing (12.5%), and two for validation (12.5%) to evaluate the network's performance. The backpropagation algorithm with a decreasing gradient, a learning rate $\eta = 0.1$, and 100 iterations was used for training the neural network. The (TRAINLM) LM algorithms were chosen for their low memory usage and speed. The tangent hyperbolic sigmoid transfer function (TANSIG) was used as the activation function.

Table 5 lists the data sets used for training and testing during model development. The results of analyzing real and projected data are shown in **Fig. 12** and **Table 3** to evaluate the effectiveness of ANN models. It was shown that the expected and actual results align well [81]. For FS, CS, and TC predicted vs. actual data, the corresponding R^2 values for the training,

validation, testing, and overall data sets are 0.9988, 0.9999, 0.9896, and 0.9888; 0.9984, 0.9999, 0.9982, and 0.9986; and 0.9963, 0.9999, 0.9946, and 0.9944. The R^2 for predicted vs. actual data on the training, validation, testing, and overall data sets for FS, CS, and TC are 0.9988, 0.9999, 0.9896, and 0.9888; 0.9984, 0.9999, 0.9982, and 0.9986; and 0.9963, 0.9999, 0.9946, and 0.9944. The high R^2 values, all above 0.97, indicate a strong correlation between experimental and expected results.

As a result, the produced ANN models (**Table 6**) could accurately predict reactions because they were based on experimental data. Error rate calculation, which measures the difference between the ANN's predictions and test results, is one of the most important parts of evaluating performance. **Figs. 13a, 13c, and 13e** show the zero-error zone, where errors are the lowest. A few errors were intentionally made to demonstrate performance during the ANN network construction phase. At the start of the ANN learning process, the MSE value increased; however, by the end, it decreased. When the best-fit line was aligned with the learning, confirmation, and testing phases, the MSE values for FS, CS, and TC decreased at the 36th, 8th, and 11th epochs, respectively (**Figs. 13b, 13d, and 13f**). After that, the ANN training process was completed. This result aligns with previous studies by other researchers, based on earlier published research on the use of ANNs [82-84]. The results show that the models can reliably predict the thermomechanical performance based on selected parameters. This research highlights the effectiveness of using RSM and ANN models to achieve specific performance goals, demonstrating their practical use in brick manufacturing.

3.4. The model's accuracy and usability

The models' validity was further evaluated by comparing the results from RSM and ANN methods. The model generated predictions that closely matched the actual data, as shown by graphs created from all test results. The RSM model's output did not fit the data or match the expected results from the ANN model. Therefore, when extrapolating datasets, the ANN model

may perform better than the RSM model. The ANN approach allows for accurate prediction and validation of experimental results to assess the thermomechanical properties of bricks. The R^2 , MSE, and RMSE metrics were used to assess the suitability of both models. The strong correlation among these metrics indicates that the models are suitable for reproducing real-world outcomes. Generally, a model with an R^2 closer to one is considered more effective at predicting responses [85]. **Table 7** shows the statistical significance and positive results of the ANN and RSM techniques in relation to the observed data. The R^2 values for the ANN model surpass those of the RSM model. Specifically, RSM yields R^2 values of 0.9769, 0.9856, and 0.9649, and MSE values of 0.3032, 0.4653, and 0.4537 for FS, CS, and TC, respectively. Meanwhile, the ANN yields R^2 values of 0.9888, 0.9986, and 0.9944, and MSE values of 0.1043, 0.0213, and 0.1165 for the same parameters. The RMSE errors were also evaluated, showing that the ANN predictions had lower RMSE values compared to the RSM when compared to the actual responses [86].

3.5. Brick Optimization Using the Response Surface Methodology (RSM)

To determine which of the FS, CS, and TC reactions was most suitable, the RSM approach was used to find optimal values for both parameters (BVW percentage and temperature). The RSM optimization method utilizes the desirability function (DF) of the Design Expert Program. A solution that meets both the lower and upper restrictions is generated through dual-goal optimization [65]. The ideal BVW content and temperature for the FS, CS, and TC results are shown in **Tables 8** and **9** as well as **Fig. 14**. The optimal answers were 1.40 MPa, 4.22 MPa, and 0.38 W/K·m for the FS, CS, and TC values. The results indicated that 4.09% and 500°C were the best values for BVW concentration and temperature, respectively.

3.6. Artificial Neural Network (ANN) and genetic algorithm (GA) technique for variable optimization in clay bricks

Genetic mechanisms and biological selection form the basis of GAs. A set of viable starting points (chromosomes) that may be evaluated based on their capacity (fitness) constitutes the first selection point. Three basic techniques used to generate a new set of potential alternatives are selection, crossover, and mutation [87]. To improve tensile characteristics and identify the optimal temperature and B/V/W percentage, this study employs a GA technique. Compared to mathematical models developed with ANNs, this approach's remarkable predictability led to its selection. The mutation, crossover, and overall population adjustment rates for the GA were 0.01, 100, and 0.70, respectively. The crossover, selection, and mutation methods were chosen using heuristic, roulette, and uniform approaches. ANN was used as a fitness indicator to determine the best options after analyzing the methods for FS, CS, and TC over 100 iterations. **Table 9** displays the optimal variable values (B/V/W content = 4% and temperature = 500°C) and the ideal responses of TC, FS, and CS, which are 0.37 W/K·m, 1.44 MPa, and 4.36 MPa, respectively. The results showed that the ANN/GA method produced the highest CS (4.36 MPa) and FS (1.44 MPa) compared to CS (4.22 MPa) and FS (1.40 MPa) obtained with RSM/DF. For both methods, the optimal B/V/W content and temperature levels were similar. The slightly better performance of ANN/GA is due to its ability to capture nonlinear and complex relationships between outcomes and input parameters. RSM/DF is recommended for faster and simpler optimization due to its basic polynomial modeling approach. Conversely, ANN/GA is better suited for complex systems requiring higher precision, as it can model nonlinear data patterns [88].

3. Conclusion

This research emphasizes the potential of bio-sourced materials as a durable building option, particularly raw earth bricks reinforced with *Vicia faba* waste and biochar made from this waste (B/V/W). It was possible to assess the effects of biochar percentage (0.5–6%) and pyrolysis temperature (300–500°C) on the thermophysical and mechanical properties of bricks using an

experimental approach with a factorial design combined with Response Surface Methodology (RSM) and Artificial Neural Network (ANN) optimization techniques. The results lead to the following conclusions:

- o The proportion of biochar significantly influenced mechanical strength. It peaked at 4% and then decreased at higher percentages due to increased porosity.
- o The biochar component greatly enhanced flexural strength, reaching 1.47 MPa at 4% B/VW and 500°C, compared to 0.5 MPa for the control bricks. Similarly, under optimal conditions, compressive strength increased from 2.20 MPa (without biochar) to 4.41 MPa, showing a notable improvement in the material's internal cohesion.
- o As biochar content increased, thermal conductivity (TC) decreased from 0.69 W/m·K to 0.36 W/m·K, indicating that its microporous structure acts as an insulating agent.
- o Using the full factorial approach, new quadratic models for mechanical strength and TC were successfully developed, with correlation coefficients (R^2) as high as 96.5%.
- o The ideal manufacturing conditions were found at 500°C and 4% B/VW using multi-criteria optimization, ensuring the best balance between heat and mechanical performance.
- o ANN proved more reliable for predicting brick properties than RSM, with models showing lower prediction errors (both Root Mean Square Error and Mean Squared Error) and higher R^2 (> 0.98).

The hybrid VW/BVW coupling increases the energy efficiency and environmental sustainability of SEBs while recycling local plant waste and helping to reduce carbon footprints, improve thermal comfort, and utilize agricultural waste in line with the circular economy concept. To verify their practical application, long-term research, life cycle analysis, full-scale validation in a Mediterranean climate, and durability testing during repeated wetting-drying cycles are required. Additionally, while the current

formulation is optimized for non-load-bearing partitions, further research focusing on the optimization of the binder matrix or compaction pressure could extend the applicability of these bricks to load-bearing masonry systems, thereby broadening their structural impact in sustainable construction.

Declarations

Ethics approval and consent to participate: Not applicable

Consent for publication: Not applicable

Data Availability Statement:

The datasets generated and/or analysed during the current study are available from the corresponding author on reasonable request.

Competing interests:

The authors declare that they have no financial interests. All authors certify that they have no other affiliations with or non-financial interest in the subject matter or materials discussed in this manuscript that could be perceived as influencing the submitted work.

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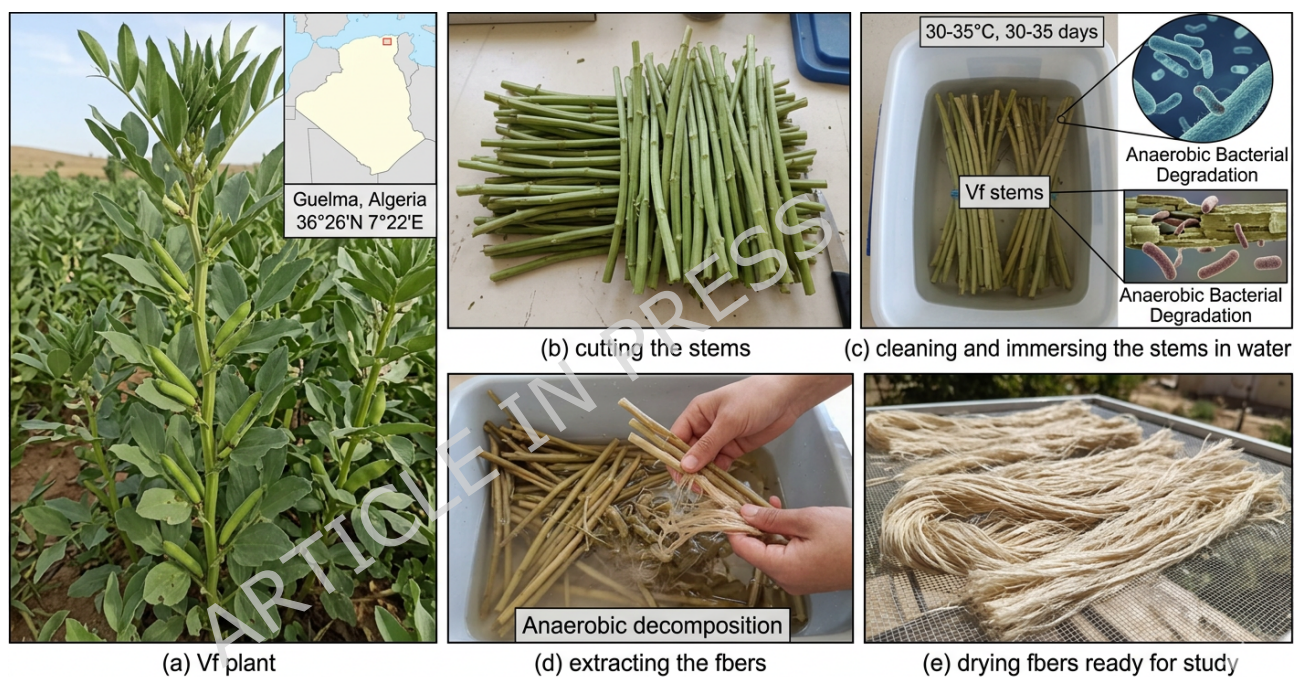


Fig. 1. Processes involved in obtaining *Vicia faba* fibers : (a) *Vf* plant; (b) cutting the stems; (c) cleaning and submerging the stems in water; (d) extracting the fibers; and (e) drying the fibers before they may be studied.

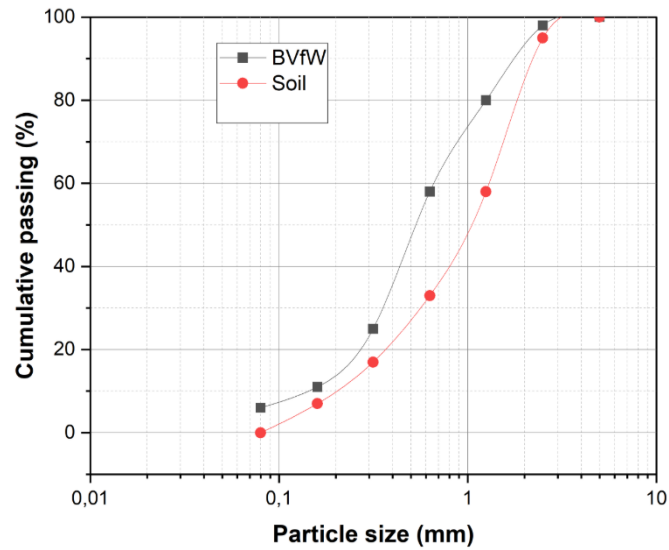


Fig. 2. Soil and biochar particle size analysis used in brick construction.



Fig. 3. (a) Raw *clay*, (b) *Vicia faba* waste (BVfW), (c) biochar made from *Vicia faba* waste (BVfW), (d) weighing of clay, biochar, and water components, (e) samples for flexural test and (f) samples for compression test.

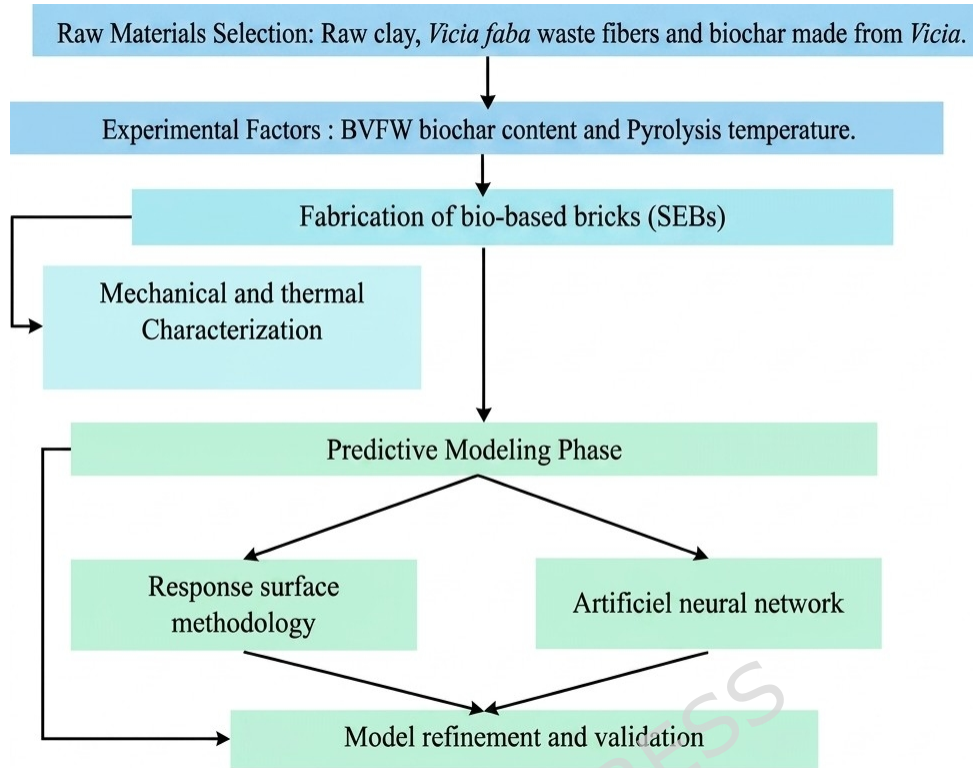
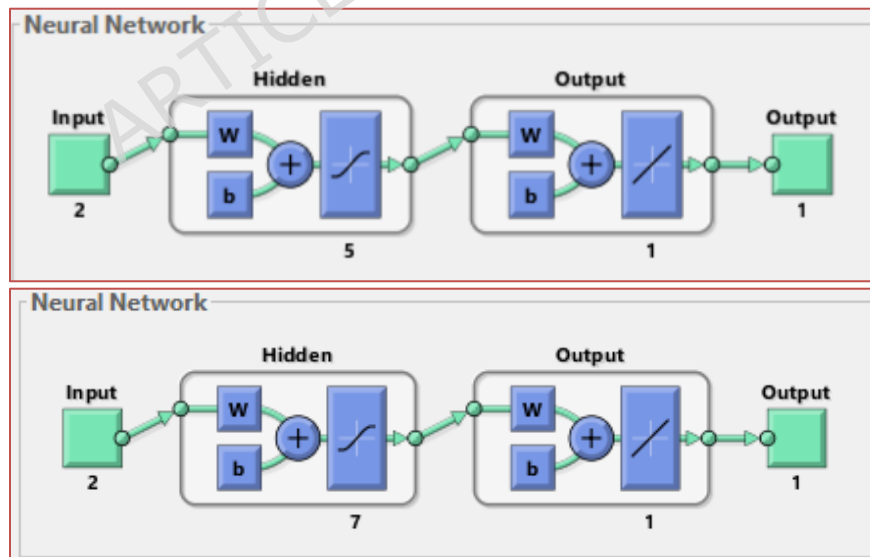


Fig. 4. Methodological framework of adobe bricks reinforced with biochar and *Vicia faba* fibres used in this study.



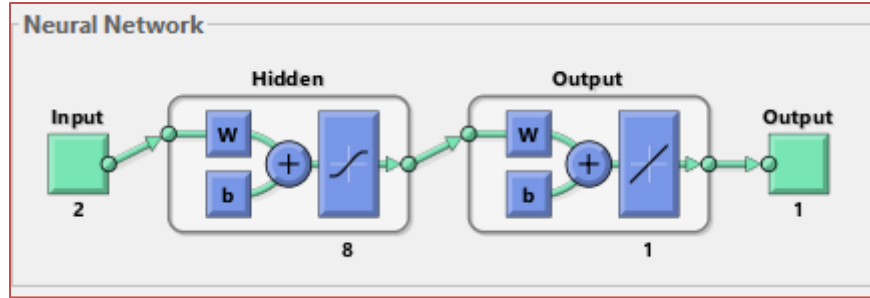


Fig. 5. Architecture of artificial neural networks (ANNs) used in this work of adobe bricks reinforced with biochar and *Vicia faba* fibres.

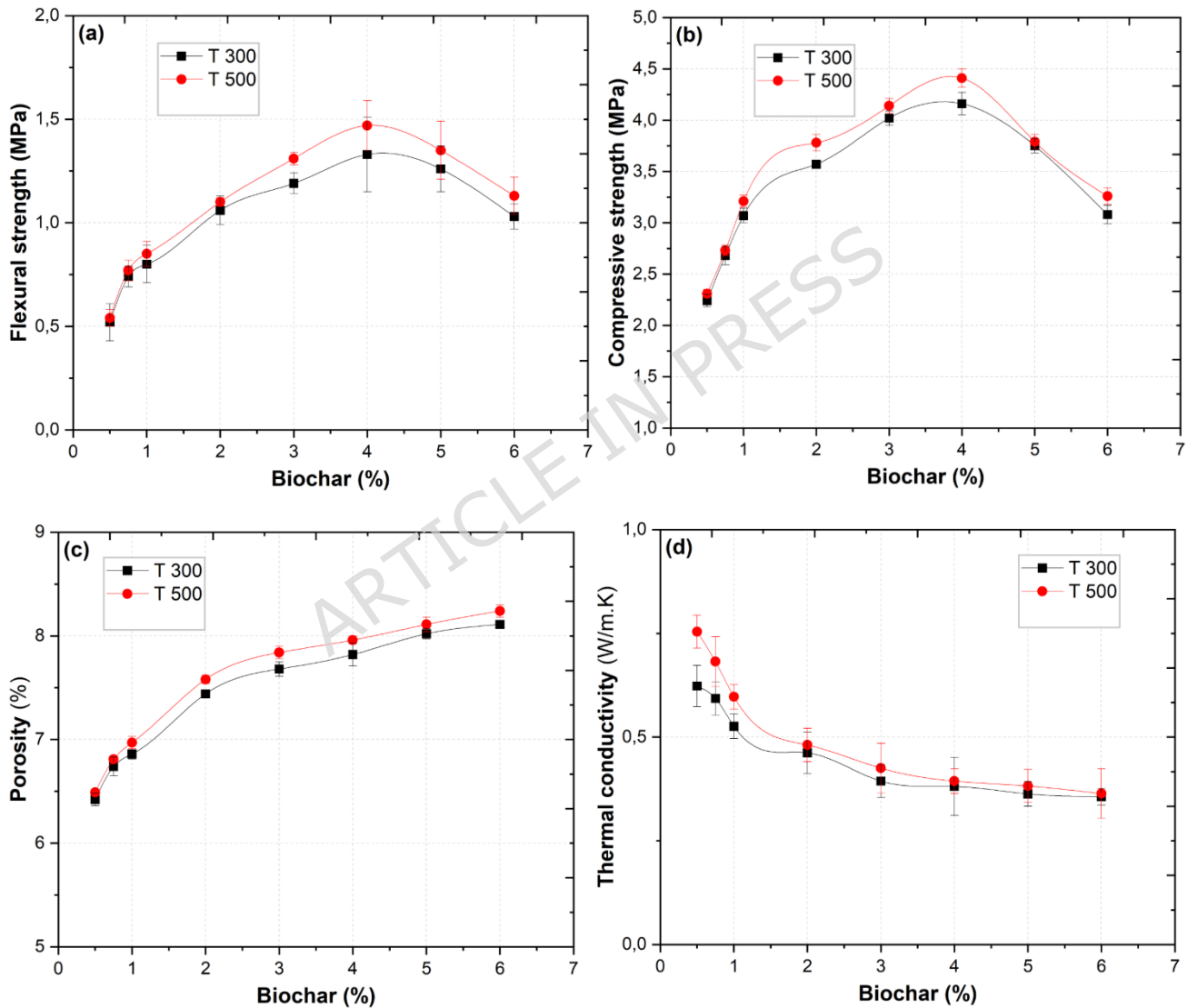
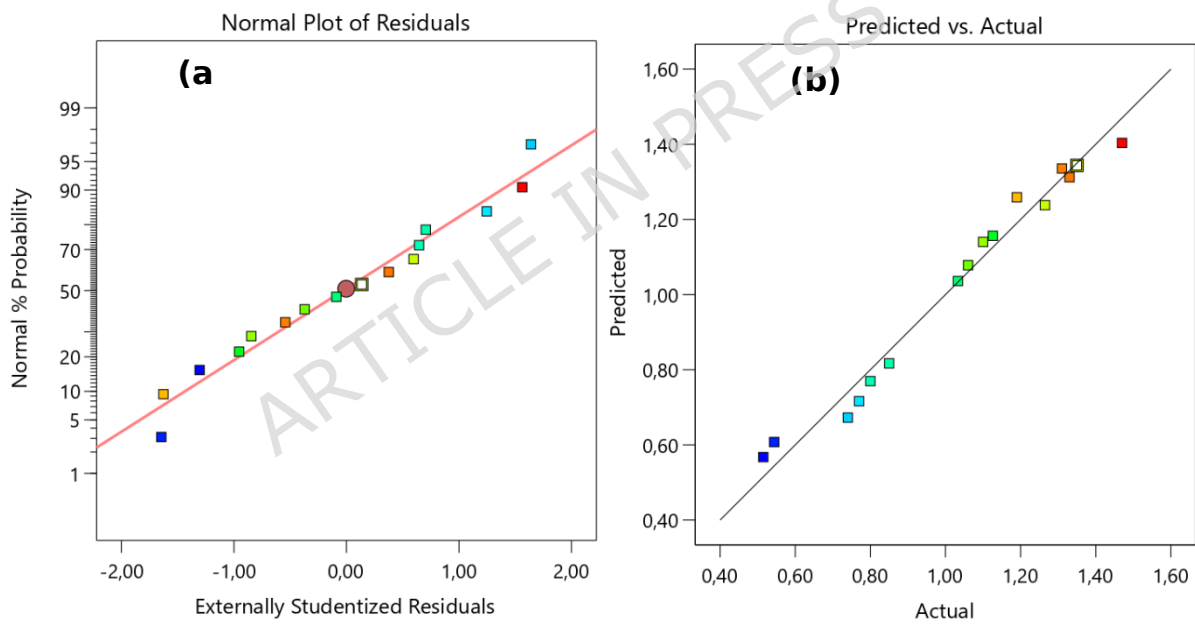


Fig. 6. Flexural strength (FS), compressive strength (CS), porosity, and thermal conductivity (TC) as functions of biochar percentage from *Vicia faba* waste (BVW) and temperature of adobe bricks reinforced with biochar and *Vicia faba* fibres.



Fig. 7. Fracture surfaces of adobe bricks reinforced with biochar and *Vicia faba* fibres.



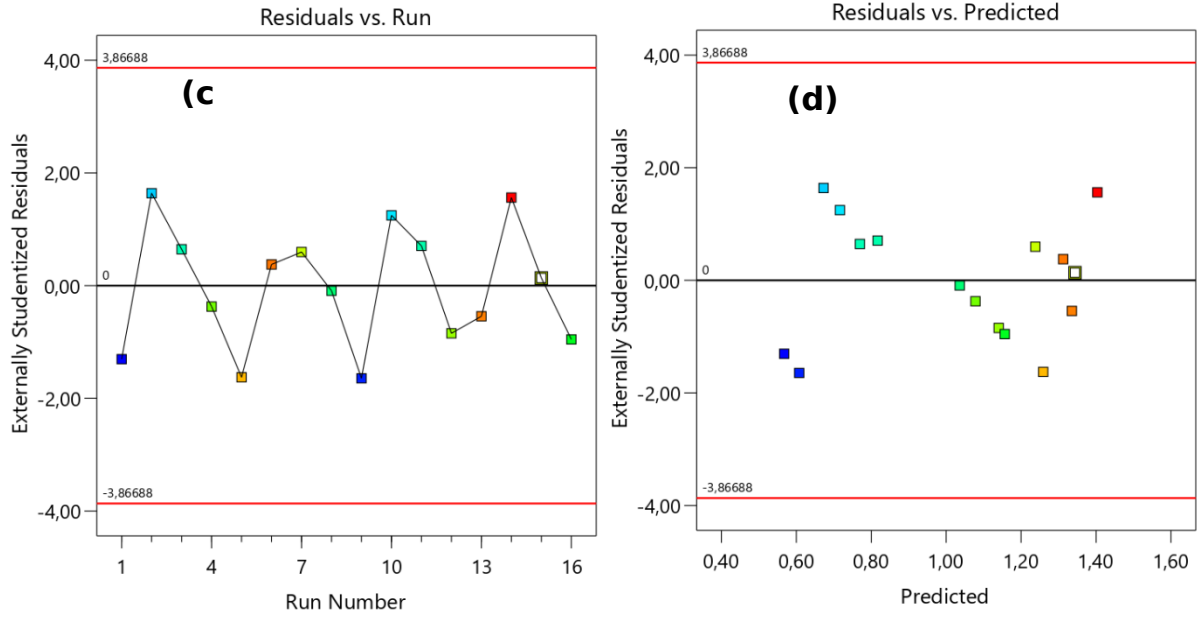
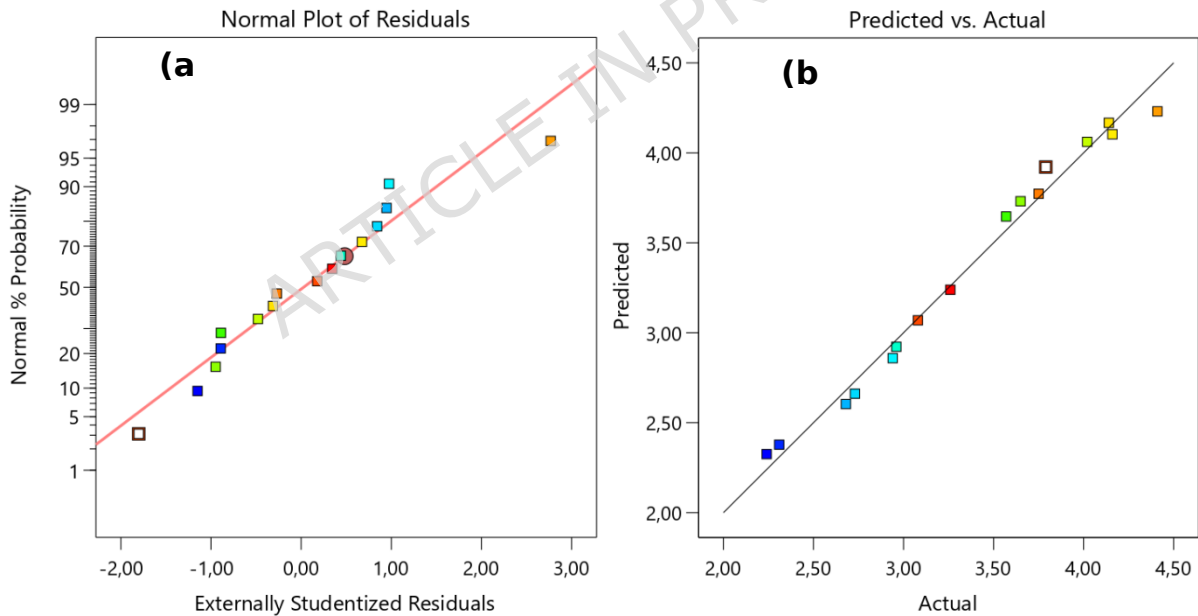


Fig. 8. Diagnosis of the bricks' flexural strength (FS) model; (a) Normal probabilities *vs.* residuals, (b) Predictions *vs.* actual values, (c) Residuals *vs.* the order of realization, and (d) Residuals *vs.* predictions.



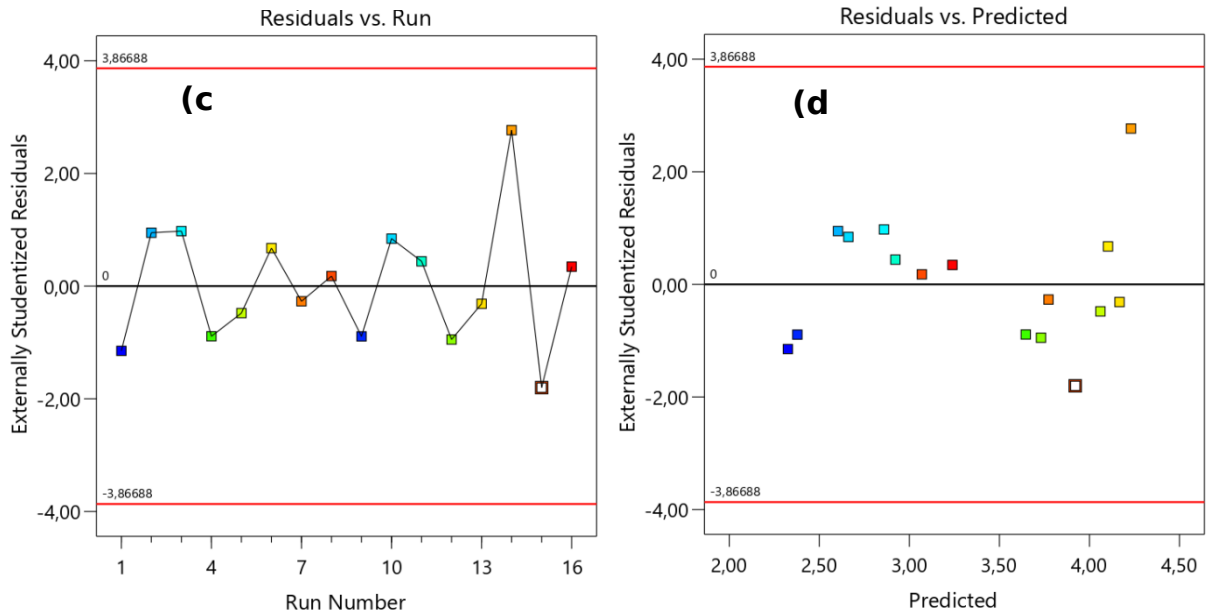
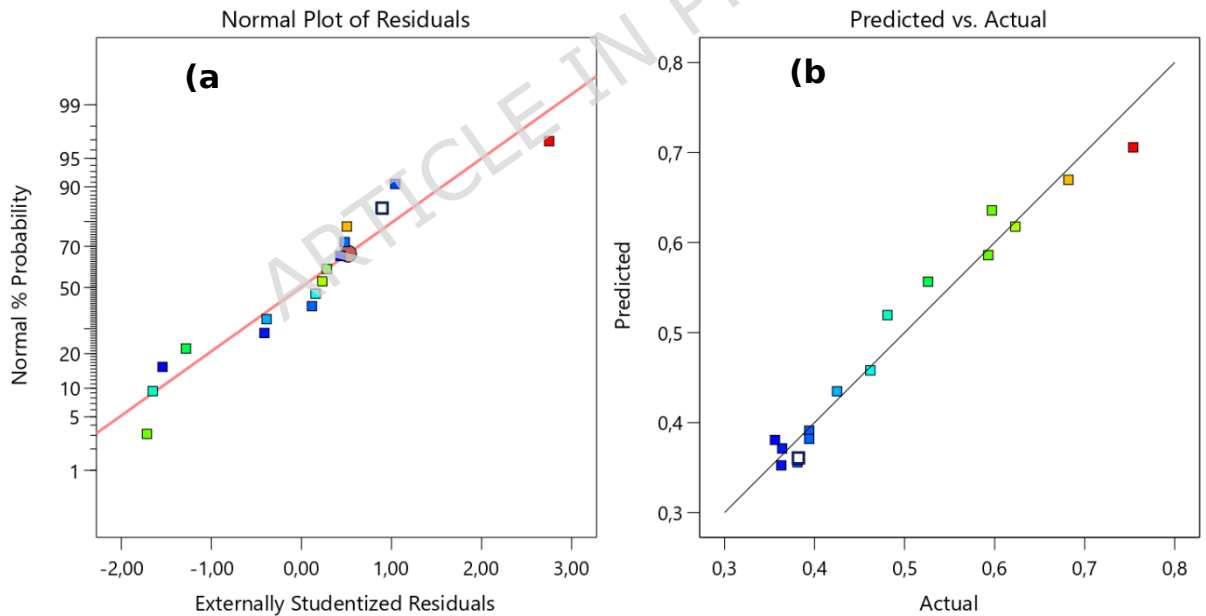


Fig. 9. Diagnosis of the bricks' compressive strength (CS) model; (a) Normal probabilities *vs.* residuals, (b) Predictions *vs.* actuals, (c) Residuals *vs.* the order of realization, and (d) Residuals *vs.* predictions.



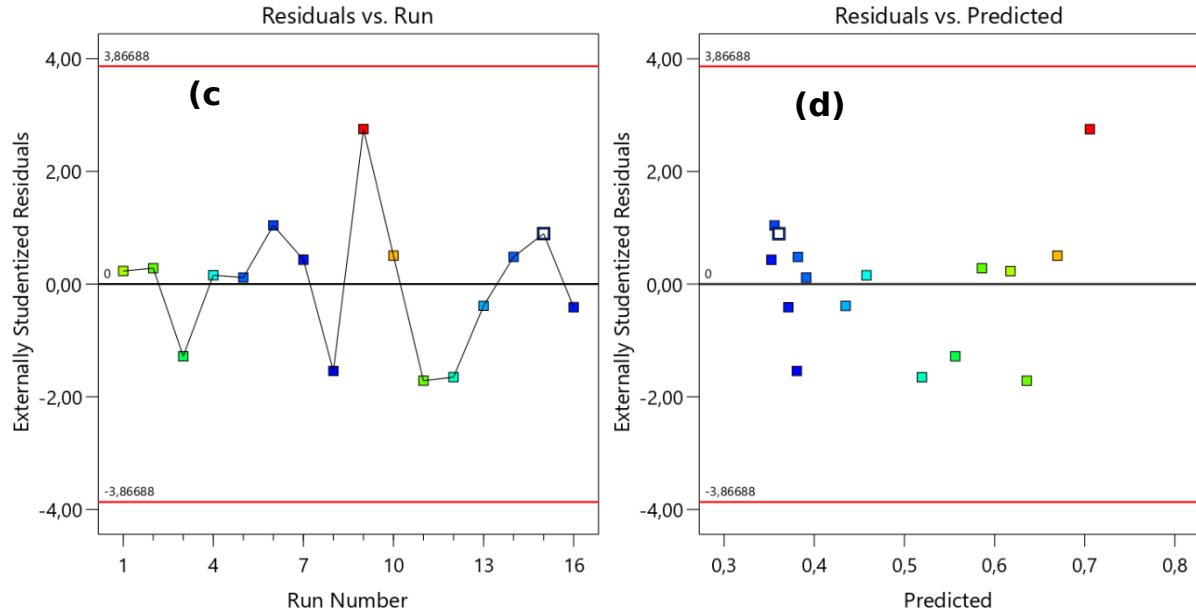
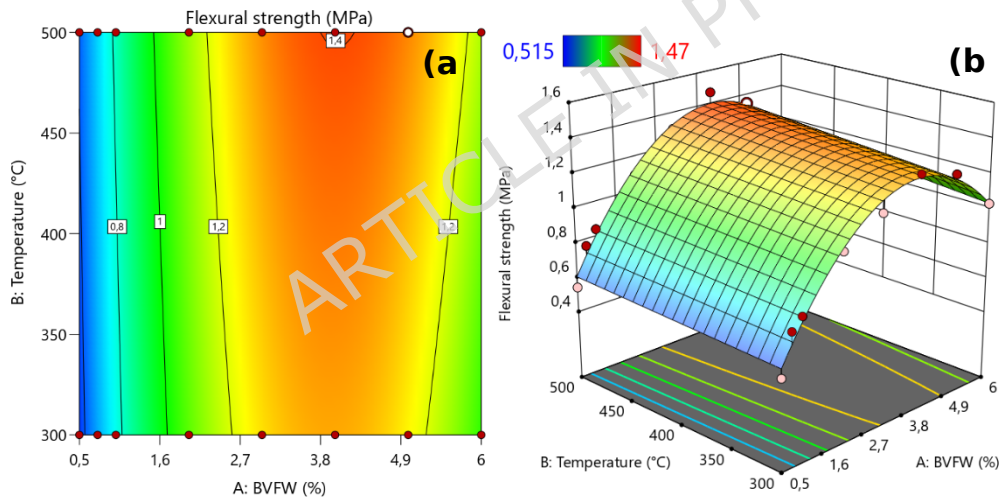


Fig. 10. Diagnosis of the bricks' thermal conductivity (TC) model; (a) Normal probabilities *vs.* residuals, (b) Predictions *vs.* actuals, (c) Residuals *vs.* the order of realization (d), and residuals *vs.* predictions.



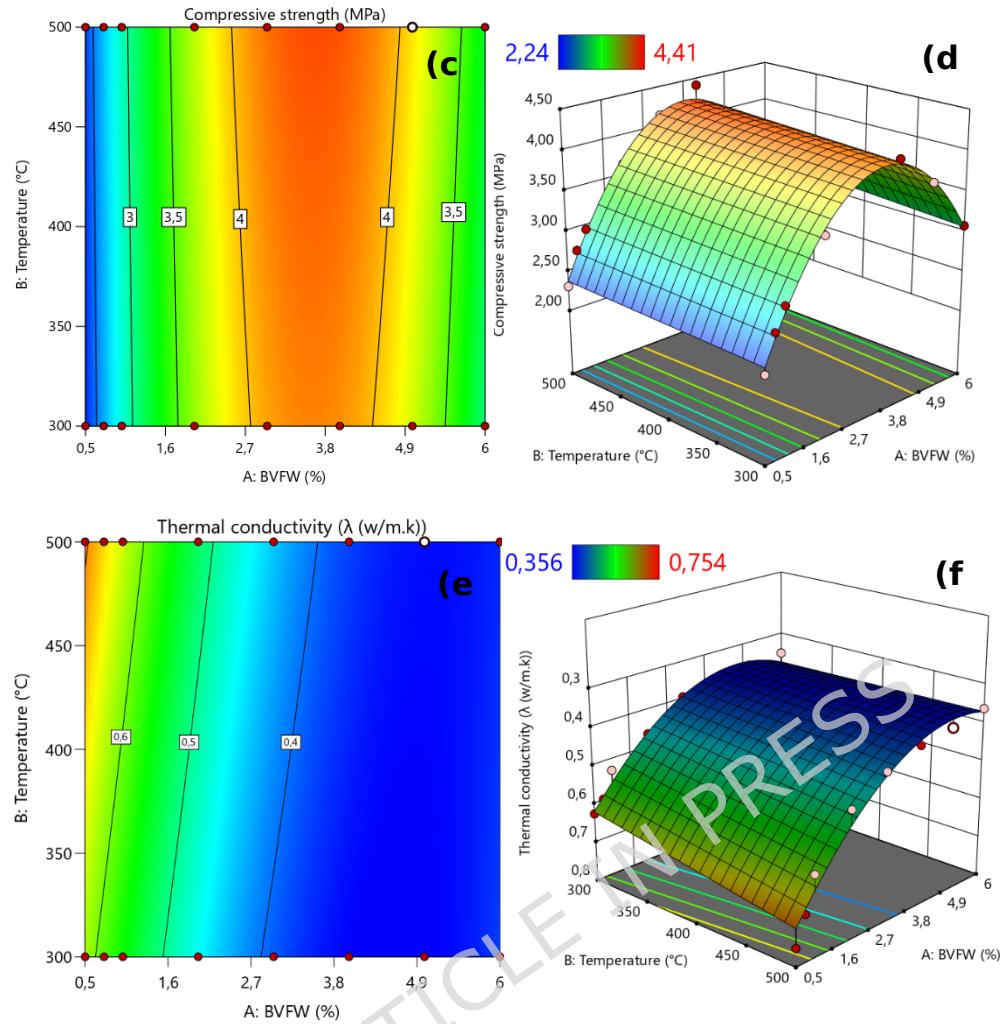


Fig.11. Contour plots and 3D response surfaces: (a, b) flexural strength (FS), (c, d) compressive strength (CS), and (e, f) thermal conductivity (TC) of adobe bricks reinforced with biochar and *Vicia faba* fibres.

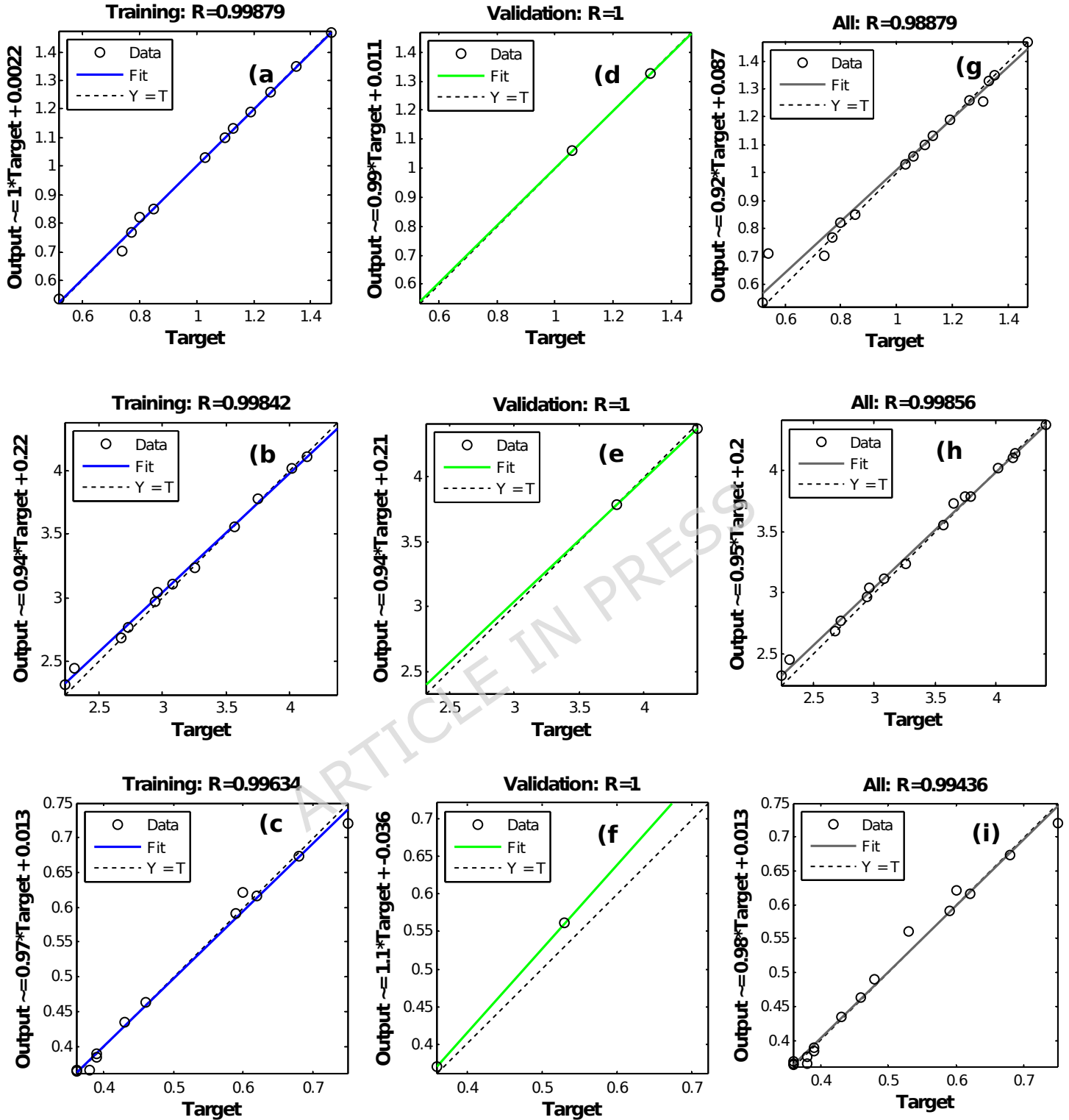


Fig. 12. Actual vs. predicted values of Artificial Neural Network (ANN) models for training (a-c), validation (d-f), and the entire dataset: (g-i) for bending strength, compressive strength (CS), and thermal conductivity

(TC), respectively of adobe bricks reinforced with biochar and *Vicia faba* fibres.

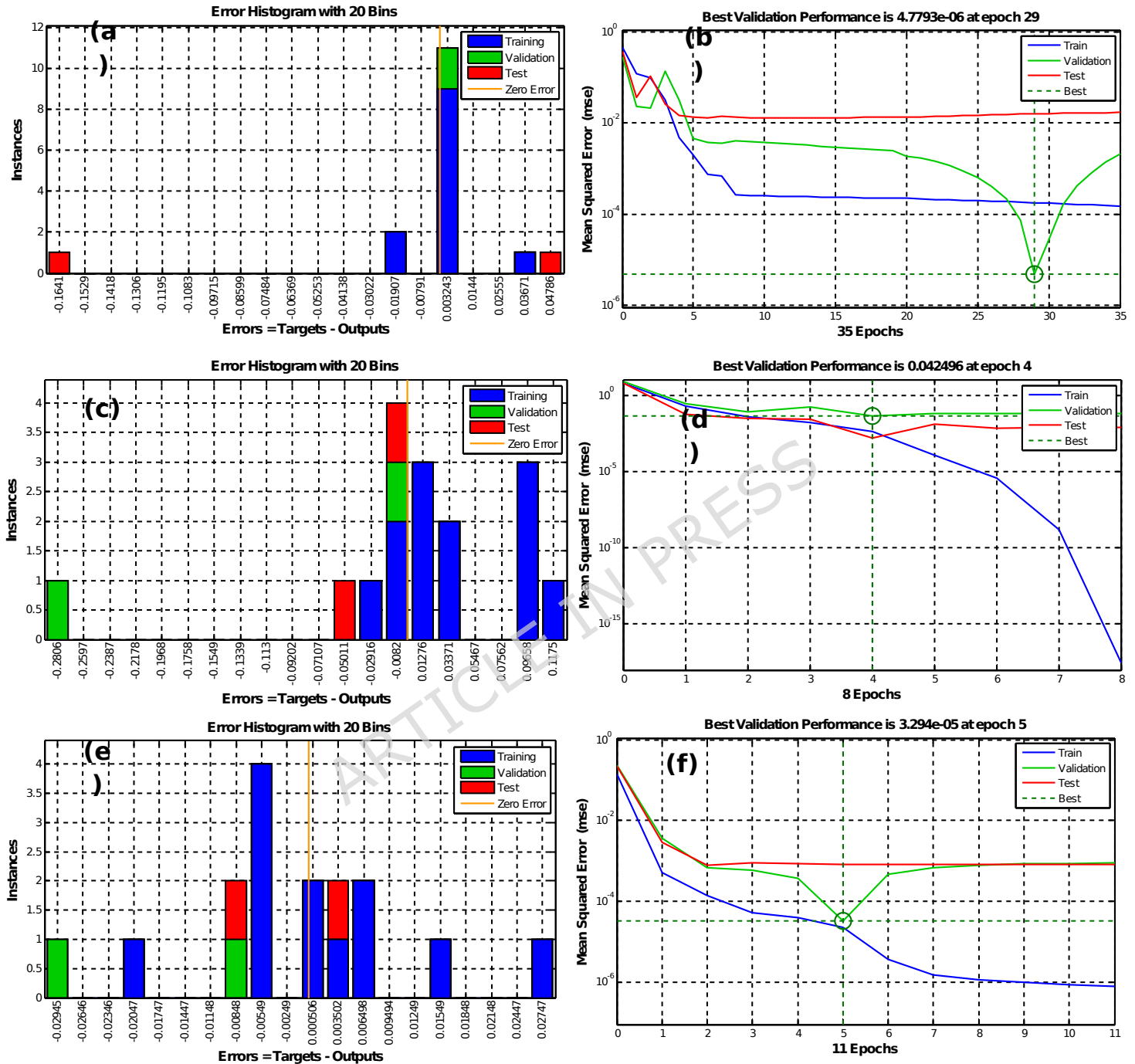


Fig. 13. Fluctuations in deviation histogram over time and mean square error for (a-b) bending strength, (c-d) compressive strength (CS), and (e-f) thermal conductivity (TC), respectively of adobe bricks reinforced with biochar and *Vicia faba* fibres.

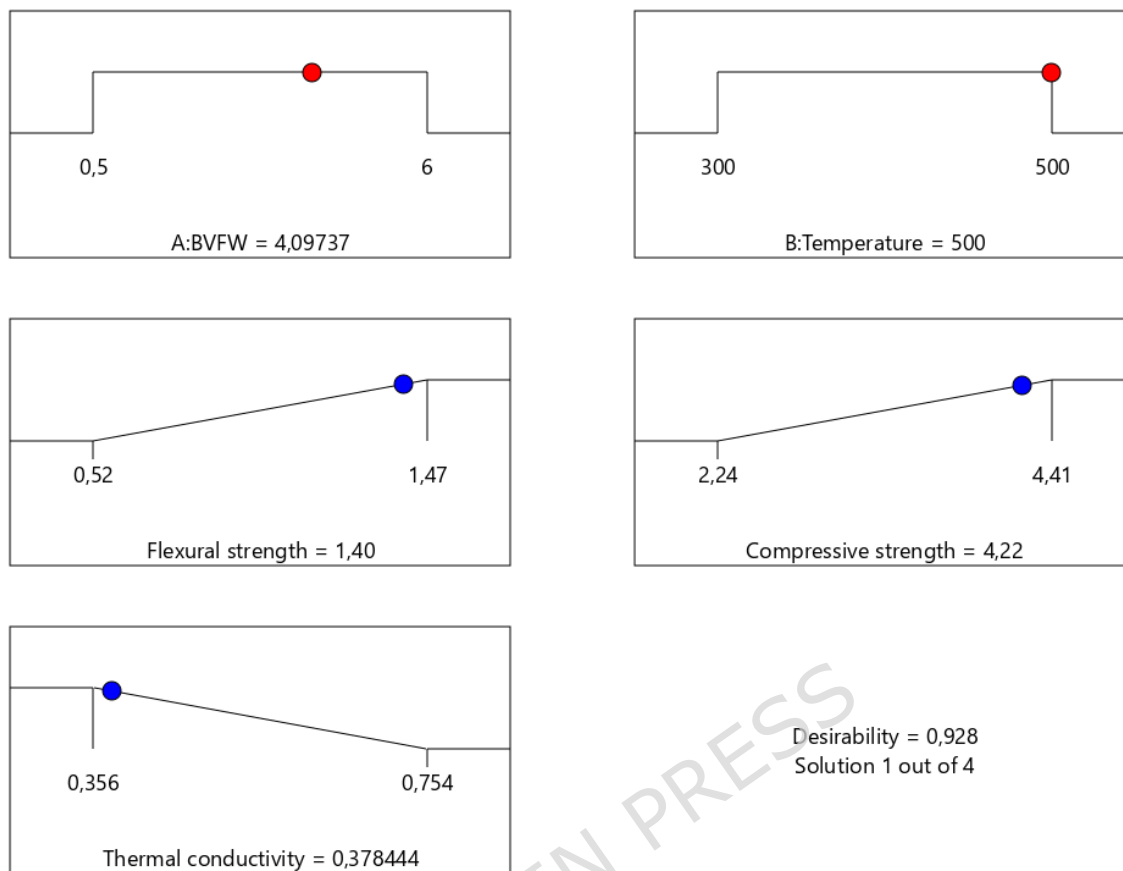


Fig. 14. Optimal responses to compressive stress, flexural stress (FS), and thermal conductivity (TC) based on predicted ramping of adobe bricks reinforced with biochar and *Vicia faba* fibres.

Table 1. Design of various process test parameters and their levels. (BVFW: Biochar derived from *Vicia faba* waste).

Factor	Unit	Symbol	Levels		
			Min (-1)	Medium (0)	Max (+1)
BVFW	%	A	0.5	3	6
Pyrolysis temperature	°C	B	300	-	500

Table 2. Bricks' values for thermal conductivity (TC), compressive strength (CS), and bending strength. (FS: Flexural strength, BVW: Biochar derived from *Vicia faba* waste).

Mixture	Factors		Responses		
	Run	A- BVW (%)	B- T (°C)	FS (MPa)	CS (MPa)
1	0.5	300	0.52±0.09	2.24±0.06	0.62±0.05
2	0.75	300	0.74±0.05	2.68±0.09	0.59±0.04
3	1	300	0.8±0.09	2.94±0.05	0.53±0.03
4	2	300	1.06±0.07	3.57±0.04	0.46±0.05
5	3	300	1.19±0.05	4.02±0.07	0.39±0.04
6	4	300	1.33±0.18	4.16±0.11	0.38±0.07
7	5	300	1.26±0.11	3.75±0.05	0.36±0.03
8	6	300	1.03±0.06	3.08±0.04	0.36±0.02
9	0.5	500	0.54±0.04	2.31±0.02	0.75±0.04
10	0.75	500	0.77±0.05	2.73±0.03	0.68±0.06
11	1	500	0.85±0.06	2.96±0.06	0.60±0.03
12	2	500	1.1±0.02	3.65±0.04	0.48±0.04
13	3	500	1.31±0.03	4.14±0.06	0.43±0.06
14	4	500	1.47±0.12	4.41±0.04	0.39±0.03
15	5	500	1.35±0.14	3.79±0.07	0.38±0.04
16	6	500	1.13±0.09	3.26±0.06	0.36±0.06

Table 3. Data on brick flexural, compressive, and thermal conductivity (TC) modeling and experiments. (RSM: Response Surface Methodology, ANN: Artificial Neural Network, FS: Flexural strength, CS: Compressive strength, BVW: Biochar from *Vicia faba* waste, EXP: Experiment).

Runs of	Input variables	Outputs		
		FS (MPa)	CS (MPa)	TC (W/m K)

experiment	A-BVW (%)	B-T (°C)	EXP			ANN			RSM		
			EXP	ANN	RSM	EXP	ANN	RSM	EXP	ANN	RSM
1	0.5	300	0.52	0.55	0.56	2.24	2.39	2.33	0.62	0.62	0.63
2	0.75	300	0.74	0.69	0.67	2.68	2.66	2.6	0.59	0.58	0.57
3	1	300	0.8	0.8	0.76	2.94	2.89	2.86	0.53	0.53	0.55
4	2	300	1.06	1.07	1.08	3.57	3.62	3.65	0.46	0.45	0.46
5	3	300	1.19	1.2	1.26	4.02	4.06	4.06	0.39	0.39	0.4
6	4	300	1.33	1.27	1.31	4.16	4.06	4.1	0.38	0.37	0.36
7	5	300	1.26	1.26	1.24	3.75	3.62	3.77	0.36	0.36	0.35
8	6	300	1.03	1.03	1.04	3.08	3.02	3.07	0.36	0.36	0.38
9	0.5	500	0.54	0.53	0.60	2.31	2.65	2.38	0.75	0.75	0.71
10	0.75	500	0.77	0.71	0.72	2.73	2.74	2.66	0.68	0.68	0.67
11	1	500	0.85	0.83	0.82	2.96	2.88	2.92	0.6	0.59	0.63
12	2	500	1.1	1.12	1.14	3.65	3.62	3.73	0.48	0.48	0.51
13	3	500	1.31	1.27	1.34	4.14	4.19	4.17	0.43	0.43	0.44
14	4	500	1.47	1.35	1.40	4.41	4.32	4.23	0.39	0.39	0.38
15	5	500	1.35	1.36	1.34	3.79	3.88	3.92	0.38	0.37	0.36
16	6	500	1.13	1.14	1.16	3.26	3.17	3.24	0.36	0.35	0.37

Table 4. Analysis of Variance (ANOVA) for thermal conductivity (TC), flexural strength (FS), and compressive strength (CS). (DF: Desirability function, MS: Mean square, CV: Coefficient of variation, R^2 : Correlation coefficient, AP: Adequate precision, SD: Standard deviation, F -value: Fisher's F statistic, BVW: Biochar derived from *Vicia faba* waste).

Source	DF	SS	MS	F -value	Prob.	Remark
a) FS						
Model	4	1.27	0.3171	116.11	< 0.0001	Significant
A-BVW	1	0.4938	0.4938	180.78	< 0.0001	
B-Temp	1	0.0243	0.0243	8.90	0.0124	
AB	1	0.0032	0.0032	1.17	0.3025	
A ²	1	0.5159	0.5159	188.88	< 0.0001	
B ²	0	0.0000		116.11	< 0.0001	
Residual	11	0.0300	0.0027			
Cor Total	15	1.30				
SD = 0.052 Mean = 1.03 CV = 5.08					R ² = 0.9769 R ² adjusted = 0.9685 R ² predicted = 0.9505 AP = 28.6106	
b) CS						
Model	4	6.79	1.70	188.84	< 0.0001	Significant

A-B VW	1	1.23	1.23	136.72	<	0.0001	
B-Temp	1	0.0468	0.0468	5.20		0,0435	
AB	1	0.0068	0.0068	0.7601		0,4019	
A ²	1	4.40	4.40	489.34	<	0.0001	
B ²	0	0.0000		14.24			
Residual	11	0.0989	0.0090				
Cor Total	15	6.89					
SD = 0.0948 Mean = 3.35 CV = 2.83					R ² = 0.9856 R ² adjusted =0.9804 R ² predicted = 0.9725 AP =35.9346		
c) TC							
Model	4	0.2358	0.0590	75.56	<	Significant 0.0001 t	
A-B VW	1	0.1558	0.1558	199.68	<	0.0001	
B-Temp	1	0.0058	0.0058	7.49		0,0194	
AB	1	0.0047	0.0047	6.02		0,0320	
A ²	1	0.0318	0.0318	40.82	<	0.0001	
B ²	0	0.0000					
Residual	11	0.0086	0.0008				
Cor Total	15	0,2444					
SD = 0.0279 Mean = 0.4861 CV = 5.75					R ² = 0.9649 R ² adjusted =0.9521 R ² predicted = 0.9170 AP =22.6245		

Table 5. Details on Artificial Neural Network (ANN) data processing. (MSE: Mean Square Error, FS: Flexural strength, CS: Compressive strength, TC: Thermal conductivity, R^2 : Correlation coefficient).

Model	Network architecture	Percentage	Samples	MSE	R^2	
FS	2-5-1	Training	70	12	1.43276E-05	0.9988
		Validation	15	2	4.17483E-04	0.9999
		Testing	15	2	3.24356E-03	0.9896
CS	2-7-1	Training	70	12	2.67832E-06	0.9984
		Validation	15	2	1.42134E-04	0.9999
		Testing	15	2	5.34528E-02	0.9982
TC	2-8-1	Training	70	12	4.65732E-04	0.9963
		Validation	15	2	2.14325E-04	0.9999
		Testing	15	2	6.38912E-05	0.9946

Table 6. Predicted values of bricks' thermal conductivity (TC), compressive strength, and bending strength generated by an Artificial Neural Network (ANN).

ANN responses	Mathematical models
Bending_strength	$1.0531 \times H1 + 0.0260 \times H2 - 0.4646 \times H3 - 2.4746 \times H4 + 0.5095 \times H5 + 0.1986$
	$H1 = \tanh(.5 \times (0.4625 \times BVfW - 0.0005 \times T + 1.3287))$
	$H2 = \tanh(.5 \times (-0.5863 \times BVfW - 0.0007 \times T + 1.1497))$
	$H3 = \tanh(.5 \times (-0.9982 \times BVfW + 0.0001 \times T - 1.1437))$
	$H4 = \tanh(.5 \times (0.1901 \times BVfW - 0.0014 \times T + 0.2591))$
	$H5 = \tanh(.5 \times (-0.0196 \times BVfW - 0.0044 \times T + 1.4647))$
Compressive strength	$0.3958 \times H1 - 0.5503 \times H2 - 0.9177 \times H3 - 0.8691 \times H4 - 0.2876 \times H5 - 0.9713 \times H6 + 0.7997 \times H7 + 2.8313$
	$H1 = \tanh(.5 \times (-0.1373 \times BVfW - 0.0119 \times T + 3.7556))$
	$H2 = \tanh(.5 \times (0.2175 \times BVfW + 0.0044 \times T - 1.2570))$
	$H3 = \tanh(.5 \times (0.4365 \times BVfW - 0.0041 \times T + 1.1178))$
	$H4 = \tanh(.5 \times (-1.0733 \times BVfW - 0.0050 \times T + 0.5429))$
	$H5 = \tanh(.5 \times (0.0381 \times BVfW + 0.0045 \times T - 0.7362))$
	$H6 = \tanh(.5 \times (-1.1705 \times BVfW - 0.0032 \times T - 0.8913))$
	$H7 = \tanh(.5 \times (-0.3509 \times BVfW + 0.0003 \times T + 0.236))$
Thermal conductivity	$-0.0291 \times H1 + -0.2066 \times H2 + -0.962466 \times H3 + -0.4351 \times H4 + 0.0065 \times H5 + -0.0666 \times H6 + -0.3989 \times H7 + -0.2818 \times H8 + 0.8503$
	$H1 = \tanh(.5 \times (0.1709 \times BVfW - 0.0105 \times T + 4.2692))$
	$H2 = \tanh(.5 \times (0.3436 \times BVfW + 0.0146 \times T - 6.9969))$
	$H3 = \tanh(.5 \times (-0.1532 \times BVfW - 0.0026 \times T + 1.8027))$
	$H4 = \tanh(.5 \times (0.3285 \times BVfW + 0.0029 \times T - 0.7858))$
	$H5 = \tanh(.5 \times (-0.2801 \times BVfW + 0.0035 \times T - 0.9641))$
	$H6 = \tanh(.5 \times (-0.7310 \times BVfW - 0.0046 \times T - 0.2158))$
	$H7 = \tanh(.5 \times (0.6050 \times BVfW + 0.0001 \times T + 1.0053))$
	$H8 = \tanh(.5 \times (-0.4280 \times BVfW - 0.0031 \times T + 1.0123))$

Table 7. Correlation coefficient (R^2), mean square error (MSE), and root mean square error (RMSE) for Flexural Strength (FS), CS, and TC as determined by Response Surface Methodology (RSM) and Artificial Neural Network (ANN).

Responses	R^2		MSE		RMSE	
	RSM	ANN	RSM	ANN	RSM	ANN
FS	0.9769	0.9888	0.3032	0.1043	0.1232	0.1106
CS	0.9856	0.9986	0.4653	0.0213	0.0645	0.0253
TC	0.9649	0.9944	0.4537	0.1165	0.4564	0.0231

Table 8. Goals and variations of optimization variables. (FS: Flexural strength, CS: Compressive strength, BVW: Biochar from *Vicia faba* waste).

Title	Objective	Lower level	Upper level
A: BVW %	In range	0.5	6
B: Temperature	In range	300	500
FS	Maximize	0.51	1.47
CS	Maximize	2.24	4.41
TC	Minimize	0.36	0.75

Table 9. Experimental results and optimization parameters. (RSM: Response Surface Methodology, DF: Desirability Function, ANN: Artificial Neural Network, FS: Flexural Strength, CS: Compressive Strength, BVW: Biochar Derived from *Vicia faba* Waste).

Name	Input variables		Responses		
	BVW content (°C)	Temperature (%)	FS (MPa)	CS (MPa)	TC (W/K.m)
Objective	In range	In range	Maximum	Maximum	Minimum
Optimization ANN/GA	4	500	1.44	4.36	0.34

Optimization RSM/DF	4.09	500	1.40	4.22	0.38
Experimental tests	4	500	1.43	4.32	0.35

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